

This Page Is Inserted by IFW Operations
and is not a part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

IMAGES ARE BEST AVAILABLE COPY.

**As rescanning documents *will not* correct images,
please do not report the images to the
Image Problem Mailbox.**

PCT

TECHNICAL LIBRARY
WORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau



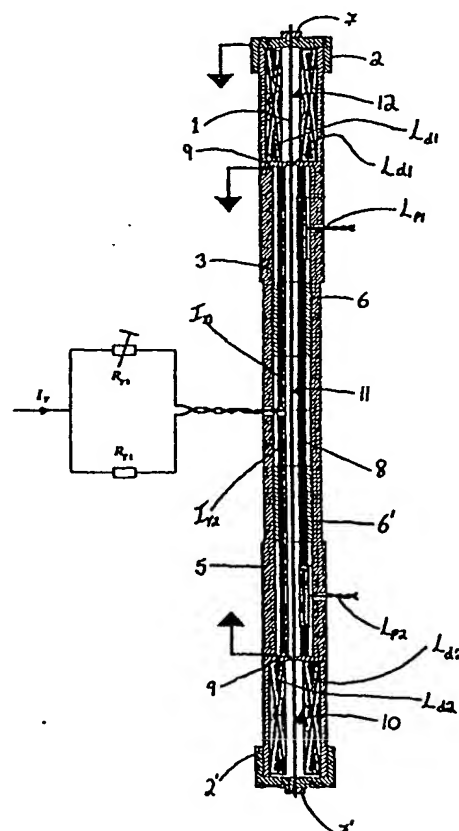
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁶ : G01V 7/00	A1	(11) International Publication Number: WO 96/10759 (43) International Publication Date: 11 April 1996 (11.04.96)
<p>(21) International Application Number: PCT/GB95/02349</p> <p>(22) International Filing Date: 4 October 1995 (04.10.95)</p> <p>(30) Priority Data: 264610 4 October 1994 (04.10.94) NZ</p> <p>(71) Applicant (for all designated States except US): GRAVITEC INSTRUMENTS LIMITED [BS/-]; Suite 5, Tower Hill House, Le Bordage, St. Peter Port, Guernsey GY1 3QT (GB).</p> <p>(71) Applicant (for MK only): TOMLINSON, Kerry, John [GB/GB]; Frank B. Dehn & Co., Imperial House, 15-19 Kingsway, London WC2B 6UZ (GB).</p> <p>(72) Inventor; and (75) Inventor/Applicant (for US only): VERYASKIN, Alexey, Vladimirovich [RU/NZ]; 1/22B Hillsborough Road, Mt. Roskill, Auckland 4 (NZ).</p> <p>(74) Agent: TOMLINSON, Kerry, John; Frank B. Dehn & Co., Imperial House, 15-19 Kingsway, London WC2B 6UZ (GB).</p>		<p>(81) Designated States: AL, AM, AT, AU, BB, BG, BR, BY, CA, CH, CN, CZ, DE, DK, EE, ES, FI, GB, GE, HU, IS, JP, KE, KG, KP, KR, KZ, LK, LR, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, TJ, TM, TT, UA, UG, US, UZ, VN, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG), ARIPO patent (KE, MW, SD, SZ, UG).</p> <p>Published With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</p>

(54) Title: APPARATUS FOR THE MEASUREMENT OF GRAVITATIONAL FIELDS

(57) Abstract

Apparatus for measuring gravitational fields comprising a superconducting string (1) fixed at both ends and forming part of a closed superconducting loop inductively coupled to two driving solenoids (L_{d1} , L_{d2}). Displacement of the string in response to a gravitational field is sensed by two magnetic flux transformers each comprising a signal coil and two pick-up coils (L_{p1} , L_{p2}). Pairs of pick-up coils lie in two perpendicular planes providing two independent channels of measurements. The two arms of each flux transformer are balanced to convert only the amplitudes of the string's antisymmetric natural modes into an output voltage. The output voltage of each channel is used to produce a feed-back current distribution (I_{y1} , I_{y2}) proximate and parallel to the string. By adjusting the feed-back current, the effective relaxation time and resonant frequency of the first antisymmetric mode of the string can be adjusted, while leaving the symmetric modes unchanged, thus increasing the apparatus' sensitivity to gravity gradients.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

- 1 -

Apparatus for the measurement of gravitational fields

5 This invention relates to the measurement of gravitational fields, particularly to gravity gradiometry, and more particularly to a method for measuring absolutely off-diagonal components of the gravity gradient tensor.

10 The gravity gradient tensor is a two-dimensional matrix of the second partial derivatives of a gravitational potential, V , with respect to the cartesian co-ordinates, x, y, z , of some arbitrary reference frame.

15 It represents how the gravity vector itself in each of these directions varies along the axes.

Accurate absolute measurements of the components of the gravity gradient tensor $\Gamma_{ij} = \partial^2_{ij}V$ ($ij = x, y, z$), taken at

20 some local coordinate frame OXYZ are very important to progress in the fields of geological prospecting, mapping of the Earth's gravitational field, and space, sea and underwater navigation.

25 A method of absolute measurement of gravity gradient tensor components was invented first by Baron Roland von Eötvös as early as 1890, utilising a torsion balance with proof masses hung at different heights from a horizontal beam suspended by a fine filament. The

30 gravity gradients give rise to differential forces being applied to the masses which result in a torque being exerted on the beam, and thus to angular deflection of the masses which can be detected with an appropriate sensor. A sensitivity of about 1 E ($1 \text{ E} = 1 \text{ Eötvös} = 10^{-9} \text{ s}^{-2}$) can be reached but measurement requires several

35 hours at a single position due to the necessity to recalculate the gravity gradient components from at least 5 independent measurements of an angular

- 2 -

deflection each with a different azimuth angle.

Practical devices, which have been built in accordance with this basic principle, are large in size and have low environmental noise immunity, thus requiring specially prepared conditions for measurements which excludes any possibility of using them on a moving carrier.

10 A method for absolute measurement of gravity gradient tensor components which enhances the above method was invented by Forward in the middle of the sixties (see US patents 3,722,284 (Forward et al) and 3,769,840 (Hansen). The method comprises mounting both a dumbbell
15 oscillator and a displacement sensor on a platform which is in uniform horizontal rotation with some frequency Ω about the axis of the torsional filament. The dumbbell then moves in forced oscillation with double the rotational frequency, whilst many of the error sources and noise sources are modulated at the rotation
20 frequency or not modulated (particularly $1/f$ noise). The forced oscillation amplitude is at a maximum when the rotation frequency satisfies the resonance condition $2\Omega = \omega_0$, where ω_0 is the angular resonant frequency, and the oscillator quality factor Q tends to infinity.
25 Unlike the non-rotating method, this method enables one to determine rapidly the quantities $\Gamma_{yy} - \Gamma_{xx}$ and Γ_{xy} by separating the quadrature components of the response using synchronous detection with a reference signal of frequency 2Ω .
30

The same principles can be directly used, as proposed by Metzger (see US patent 3,564,921), if one replaces the dumbbell oscillator with two or more single
35 accelerometers properly oriented on such a moving platform. There are no new features of principle in this solution to compare with the previous one except that the outputs of the pairs of accelerometers require

- 3 -

additional balancing.

Devices have been built according to this method, but they have met more problems than advantages, principally because of the need to maintain precisely uniform rotation and the small displacement measurement with respect to the rotating frame of reference. The devices have reached a maximum working accuracy of about a few tens of Eötvös for a one second measuring interval, and they are extremely sensitive to environmental vibrational noise due to their relatively low resonant frequencies. The technological problems arising in this case are so difficult to overcome that the existing developed designs of rotating gravity gradiometers are so far only at the stage of prototypes whose measurement accuracy is much lower than the limiting theoretical estimates.

In a paper by A. Nicolaidis and A. Taramopoulos (Il Nuovo Cimento, Vol. 107B, N.11, pages 1261-1266, November 1992), the theoretical motion of a string with fixed ends under the influence of a plane monochromatic time-varying gravitational wave is discussed. According to this document, a string with fixed ends may be excited to resonance provided certain conditions, dependent on the length and orientation of the string and the wavelength of the gravitational wave, are met. It is suggested that Fourier analysis of the motion of the string could be used to extract the direction and energy of the incident wave. The document specifically avoids any discussion of the technical implementation of the theory, but it does suggest that strings a few metres or a few kilometres long should be used for the detection of cosmological radiation or gravitational radiation from a black hole or supernova, as the length of the string should be comparable to the wavelength of the gravitational waves. For the theoretical detector to work requires the gravitational field to oscillate in

- 4 -

the form of a gravitational wave, which would not be the case for the gravitational fields associated with massive bodies such as the Earth.

5 Superconducting gravity gradiometers are known (see US patent 4,841,772 and Australian patent application 48185/90) utilising a pair or more of sufficiently separated superconducting accelerometers. Even after greatly reducing the intrinsic and environmental thermal
10 noise factor, using stable persistent super-currents to balance the outputs of the accelerometers, and the most sensitive displacement sensors based on SQUIDS (Superconducting Quantum Interference Devices), they cannot measure the gravity gradient tensor components in
15 their absolute units because they are incapable of fixing a position of the accelerometer's proof mass which is free of all forces. Therefore, only relative displacements of the proof masses can be measured. Rotating designs of such superconducting gravity
20 gradiometers are not known.

It is an object of the present invention to provide an apparatus for the measurement of gravitational fields with improved sensitivity, portability and noise
25 immunity over the above known systems.

It is a further object of the present invention to provide a novel apparatus for the absolute measurement of off-diagonal components of the gravity gradient
30 tensor, in which the effect of rotation is replaced by parametric interaction between the sensitive element and active force feed-back connections, whereby enhanced sensitivity and vibrational noise immunity are attained.

35 It is another object of the present invention to provide a simple technological realisation of the above apparatus utilising the advantages of the standard superconducting techniques which have shown an ability

to reach a maximum sensitivity for mechanical displacement measurements and to keep intrinsic noise at a minimum level.

- 5 To achieve these objects the present invention provides an apparatus for the measurement of quasi-static gravitational fields, comprising:

10 a string fixed at both ends and held under tension; sensing means for detecting the transverse displacement of said string from an unperturbated position, due to a gravitational field acting on said string;

and means responsive to the detected displacement for producing an output which is a function of the gravitational field.

15

By "string" no particular limitation as to material or construction is intended. Any elongate tension element is included which is capable of being transversely deflected by a gravitational field and of providing a

20

An unperturbated stretched flexible string with fixed ends forms an absolute straight line in space going through the points where the ends of the string are

25 fixed. This line can be identified as one of the axes of the local coordinate frame, say Z, and the other two axes, X and Y, are chosen to lie in the transverse (to the string) plane. Any string deflection from this line is caused by absolute values of the transverse

30 components of the force per unit length which is applied to each unit element of the string.

- 35 Viewed from another aspect the invention provides a method of measuring quasi-static gravitational fields, comprising:

providing a string with fixed ends and held under tension;

detecting the transverse displacement of said

- 6 -

string from an unperturbated position due to a gravitational field acting on said string; and

producing an output in response to the detected displacement, said output being a function of said gravitational field.

The string's deflection from its unperturbated position can be easily detected, by any suitable displacement sensing device.

Preferably the string is formed of conductive, most preferably superconductive material. In this case, if an electric current flows through the string, a magnetic field distribution is produced in the transverse plane and along the string's direction. If the string is made of a superconducting material, a maximum current can be carried, and a consequent maximum sensitivity to the deflection can be reached. A d.c. or an a.c. current may be produced in the string by incorporating the string into a current-carrying circuit directly or by an inductive coupling with a pumping circuit(s), provided that the string forms part of a closed conducting or superconducting loop. An a.c. current may be induced in the string, for example by means of one or more, preferably longitudinally symmetrically positioned, coils, which may possibly be superconducting. The use of an a.c. current is advantageous in that it allows synchronous detection of the output signal.

When the string carries a current, the transverse magnetic field around the string may interact with other conductors, or superconductors, by inductive coupling. The amplitude of the current induced in a conductor adjacent the string will be directly related to the distance of the string from that conductor. Thus, in a preferred embodiment of the invention one or more fixed pick-up coils are arranged along the length of the string to act as displacement sensing means, the current

- 7 -

induced in each coil being directly related to the string's displacement from its unperturbed position.

5 In a preferred embodiment of the invention the sensing means comprises at least two sensors, possibly pick-up coils, positioned symmetrically, in the longitudinal direction, with respect to the mid point of the string.

10 In a particularly advantageous embodiment, displacement sensors, for example pick-up coils, are arranged adjacent the string in two non-parallel preferably orthogonal, planes, so as to be capable of measuring the string's displacement in two transverse directions simultaneously.

15 It will be understood that the displacement of a string of length l from its unperturbed position, for example, in the y -direction of the above local coordinate frame as a function of the z -position of a unit element and
20 time, $y(z, t)$, can be described by the following differential equation

$$\eta \frac{\partial^2}{\partial t^2} y(z, t) + h \frac{\partial}{\partial t} y(z, t) - Y A \frac{\Delta l}{l} \frac{\partial^2}{\partial z^2} y(z, t) - \eta g_y(0, t) - \eta \Gamma_{yz}(0, t) z + \bar{f}_L(z, t) = 0 \quad (1)$$

25 with boundary conditions corresponding to the fixed ends of the string, i.e. $y(0, t) = y(l, t) = 0$. In this equation η denotes the string's mass per unit length, h is the friction coefficient per unit length, the parameters Y , A and $\Delta l/l$ are the string's Young modulus, the area of its cross section and the string's strain
30 respectively. The quantities $g_y(0, t)$ and $\Gamma_{yz}(0, t)$ are the absolute values of the y -component of the total acceleration and the corresponding gravity gradient tensor component along the string, both taken at the
35 centre of the local coordinate frame chosen. The function $\bar{f}_L(z, t)$ represents the Langevin random force

- 8 -

per unit length acting on the string due to its interaction with the thermostat having the absolute temperature T , with the following correlation function

$$\langle \tilde{f}_L(z, t) \tilde{f}_L(z', t') \rangle = 4k_B T \delta(z - z') \delta(t - t') \quad (2)$$

where $k_B = 1.4 \cdot 10^{-23} \text{ JK}^{-1}$ is the Boltzmann constant and $\delta(x - x')$ is the delta-function.

In this description, the y -direction has been chosen as an arbitrary example to simplify the explanation of the invention. However, the foregoing and following analysis is equally applicable to any direction transverse to the string or any number of directions.

Applying Fourier analysis to the complex shape of the string caused by its interaction with the gravitational field, the function $y(z, t)$, can be described, in the range $z=0$ to $z=l$, by an infinite sum of sinusoidal functions of period $2l$, with appropriate coefficients $c_y(n, t)$. Thus a solution of Eq.(1), which satisfies the boundary conditions shown above, can be represented by the following sum wherein each term in n corresponds to one of the string's natural vibrational modes

$$y(z, t) = \sum_{n=1}^{\infty} c_y(n, t) \sin\left(\frac{\pi n}{l} z\right) \quad (3)$$

By substituting Eq.(3) into Eq.(1) and by multiplying its left-hand and right-hand sides by $\sin(\pi n' z/l)$, and then by integrating both sides over z from 0 to l , one can obtain the differential equation for $c_y(n, t)$

$$\begin{aligned} \frac{d^2}{dt^2} c_y(n, t) + \frac{2}{l} \frac{d}{dt} c_y(n, t) + \omega_n^2 c_y(n, t) = \frac{2}{\pi n} [(-1)^n - 1] g_y(0, t) \\ + (-1)^n \frac{2l}{\pi n} \Gamma_{yz}(0, t) \\ + \frac{2}{\pi l} \int_0^l dz \tilde{f}_L(z, t) \sin\left(\frac{\pi n}{l} z\right) \end{aligned} \quad (4)$$

where the quantities

$$\omega_n = \frac{\pi n}{l} \sqrt{\frac{Y \Delta l}{\rho l}} \quad (5)$$

5

represent the string's natural frequencies; τ and ρ are the relaxation time and the volume mass density of the string respectively.

10

When n takes an even value, i.e. for those terms of the infinite sum in Eq. 3 corresponding to vibrational modes of the string having a node at $z=l/2$ (antisymmetric modes), the term involving $g_y(0, t)$ is equal to zero.

15

Thus, for n even, c_y is dependent only on Γ_{yz} (and thermal noise).

20

In practice this means that the amplitude, c_y , of the antisymmetric sinusoidal components of the deflection of the string in the y -direction, $y(z, t)$, is dependent only on the magnitude of the gravity gradient tensor component Γ_{yz} .

25

The mid point of the string, $z=l/2$, is the position of a node in all antisymmetric vibrational modes of the string. If sensors are positioned symmetrically in the longitudinal direction with respect to this point, it will be possible to identify displacements of the string corresponding to the string's natural antisymmetric vibrational modes while discounting displacements corresponding to symmetric modes, the magnitude of which is not only affected by the gravity gradient tensor component Γ_{yz} but also the absolute acceleration due to gravity in the y -direction, g_y .

30

35

It is particularly advantageous if displacement sensors are positioned at $z=l/4$ and $z=3l/4$, positions corresponding to the antinodes of the first

- 10 -

antisymmetric vibrational mode of the string, $n=2$. At these points the displacement of the string corresponding to the $n=2$ mode is at a maximum and thus the sensing signal will also be at a maximum, giving optimum sensitivity.

According to a further development of the invention a conductor may be provided adjacent the conductive string. The conductor may carry a current directly related to the output of the sensing means, by the use of a positive feedback loop. The current may be activated continuously or periodically, for example in an "off-on" manner. In this case, a small deflection of the string due to a gravitational field will be amplified by the magnetic interaction of the string and conductor. In other words, the conductor will "push" (or "pull") the string into further deflection in direct response to a small deflection caused by a gravitational field acting on the string. This is clearly advantageous in that the displacement of the string is greater by virtue of the magnetic interaction with the conductor and is therefore more readily measurable, improving the sensitivity of the apparatus.

In a particularly advantageous embodiment of this development, two or more conductors, possibly superconductors, are positioned longitudinally symmetrically about the mid-point of the string so that they amplify the antisymmetric modes of the string.

In overview, a preferred embodiment of the invention provides a novel apparatus for measuring absolutely and simultaneously a pair of off-diagonal components of the gravity gradient tensor by means of a flexible superconducting current-carrying string with fixed ends, comprising active parametric force feed-back connections. The string is the coherent sensitive element whose symmetric natural transverse modes are

- 11 -

caused by the total acceleration in the transverse plane, whilst the antisymmetric modes are caused only by absolute values of the gravity gradient components along the string's direction.

5

In this embodiment the string forms a low-inductance part of a closed superconducting loop which is inductively coupled to a high-inductance driving solenoid(s) carrying an a.c. reference current from an external pumping source with some frequency Ω . The string is also inductively coupled to two superconducting magnetic flux transformers each comprising a signal coil and two pick-up coils wherein the pairs of pick-up coils lie in two perpendicular planes the cross-line of which coincides with the unperturbated string, thus forming two independent channels of measurements. The two arms of each superconducting flux transformer are balanced to convert only the string's antisymmetric natural modes into signal current in the signal coil to be measured with SQUID's (Superconducting Quantum Interference Devices) electronics. The output voltage of each channel, deeply modulated with the frequency Ω , is then proportional to the amplitudes of the antisymmetric natural modes of the string. This voltage is passed through a differentiating and summing amplifier, and then used to load the feed-back circuit to produce an in-line feed-back current distribution proximate and parallel to the string. By adjusting the feed-back current, the effective relaxation time and the resonant frequency of the first antisymmetric natural mode of the string (whose amplitude depends only upon the gravity gradient along the string's direction) can be increased and decreased respectively, while the same parameters for the symmetric natural modes (whose amplitudes depend upon the total acceleration in the transverse-to-string plane) are not changed. In use, the feed-back circuit shifts the Brownian and vibrational noise level to far

10

15

20

25

30

35

- 12 -

below the sensitivity required for industrial applications.

5 A preferred embodiment of the invention will now be described by way of example only and with reference to the following drawings in which:

10 Fig. 1 is a general schematic representation of a preferred embodiment of the invention; and

Fig. 2 is a diagrammatic vertical cross-section of a device according to a preferred embodiment of the invention.

15 A single channel prototype of a device according to the invention (see Fig.2) has a flexible string 1. The string is preferably formed of a superconducting material such as Niobium (Nb). Niobium wire is the best
20 choice, having optimum elastic properties, which have been proven to be usable at 4.2 K. The string forms the low-inductance part L_0 of a superconducting closed loop which is inductively coupled to high-inductance driving solenoid(s) L_d carrying an a.c. reference current $I_d(t)$ from an external pumping source with some frequency Ω .
25 The rest of the loop is provided by the casing of the device 2,2',3,4,5.

The string has, in this embodiment, a length $l = 24$ cm, is 1 mm in diameter and is fixed at its ends by two Nb
30 cups 2,2' of cylindrical shape each having a hole of 1 mm diameter at its centre. The cups 2,2' close tightly the ends of a Nb cylinder comprising three parts 3,4,5 connected together with two Nb cylindrical rings 6,6' carrying a fine thread. The parts 3 and 5 also carry
35 threads to engage other elements of the construction. The string's tension is produced by two Nb nuts 7,7' of 1 mm fine thread.

- 13 -

The whole construction forms a closed superconducting cylindrical cavity with the string axially positioned. There are three spaces 10, 11, 12 inside this volume. electromagnetically insulated as much as possible from each other by Nb partitions 9. In two of them 10, 12, driving toroidal solenoids L_{d1} and L_{d2} , wound with 0.01 mm Nb wire and connected in series, are placed, thus forming a large mutual inductance M_d between $L_d = L_{d1} + L_{d2}$ and the inductance of the cylindrical cavity L_0 which is of the order 10^{-7} H for the sizes chosen. The ratio M_d/L_0 is about 5×10^2 , so if the a.c. pumping current $I_d(t)$ in the driving solenoids has an amplitude of about 100 mA then the induced a.c. supercurrent I_0 carried by the string is about 50A peak to peak. In this case, the corresponding circular component of the magnetic induction B at the string's surface is nearly 200 Gauss which is approximately four times smaller than the Niobium first critical field B_{c1} .

The two rectangular-type pick-up coils L_{p1} and L_{p2} of the superconducting flux transformer, and the active force feed-back circuit are mounted together on a Titanium tube 8 placed inside the central space of the construction shown in Fig.2. Titanium is chosen because it has a thermal expansion coefficient matching that of Niobium. The active force feed-back circuit comprises two arms of 0.5 mm insulated copper wire stretched parallel to the string and carrying the feed-back current $I_y = I_{y1} + I_{y2}$.

This design has particular advantages; for instance, the closed superconducting configuration gives optimum shielding against external varying electromagnetic fields. Also, the cylindrically symmetric configuration has a small radial size which, including all integral parts of the prototype, is no more than 3.8 cm diameter. Thus, it is possible to utilise a standard commercial 100 litre liquid helium vessel having an input opening

- 14 -

of about 4 cm diameter to cool the construction down with a standard probe. Special helium cryostats, which have been used for known devices, exclude the possibility of removing the device from the cryostat's inner volume, for example if something goes wrong, to readjust it under field conditions. Removal of a device from a cryostat requires a long period, of for example several hours, to warm the cryostat contents to atmospheric temperature so that the contents do not explode under rapid thermal expansion. This is one of the major disadvantages of known constructions. However, the small input opening of the standard commercial 100 litre liquid helium vessel prevents such an explosion occurring, which means that the apparatus according to the present invention can be removed from the vessel and adjusted under field conditions.

The string is deflected by a non-uniform quasi-static gravitational field and interacts with a variable feed-back current distributed close to and substantially parallel to the string. The distribution is optimum when the feed-back current is injected at or taken from the point in the feed-back circuit opposite the mid-point of the string (see Fig. 1). In the local coordinate frame chosen this point is $z = l/2$. Another requirement for optimum operation is that the two arms of the feed-back circuit are substantially equal and grounded at their ends. In this case, there is no electromagnetic coupling between the feed-back current and the closed superconducting loop in which the string is incorporated.

The current $I_0(t)$ flowing through the string and interacting with the feed-back current distribution $I_y(z, t)$ gives rise to the following transverse component of the force per-unit-length $f_y(z, t)$ acting on the string

- 15 -

$$f_y(z, t) = \pm \frac{\mu_0}{2\pi d} I_0 I_y(z, t) \sin(\Omega t) \quad (6)$$

where $\mu_0 = 4\pi \cdot 10^{-7} \text{ Hm}^{-1}$ is the magnetic vacuum permeability, d is the distance between the centre of the unperturbed string and the centre of the wire carrying the feed-back current and the phase of the pumping current source 15 is chosen to be zero. The sign + or - is determined by the output buffer of the differentiating and summing amplifier 16 shown in Fig.1. The transverse motion of the unit element of the string in the OYZ plane is then described by the following differential equation

$$\begin{aligned} 15 \quad \eta \frac{\partial^2}{\partial t^2} y(z, t) + h \frac{\partial}{\partial t} y(z, t) - Y_{nb} A \frac{\Delta l}{l} \frac{\partial^2}{\partial z^2} y(z, t) \\ - \eta g_y(0, t) - \eta \Gamma_{yz}(0, t) z \pm \frac{\mu_0}{2\pi d} I_0 I_y(t) \sin(\Omega t) + \tilde{f}_L(z, t) \end{aligned} \quad (7)$$

20 which will be seen to correspond to Eq.(1) with the addition of the term of Eq.(6). Consequently, Eq.(7) also has solutions of the form of Eq.(3). Thus, following the same algebraic manipulation as for Eq.(1), a differential equation for $c_y(n, t)$ can be obtained for this embodiment. This is Eq.(8) which corresponds to Eq.(4) but with the addition of a feedback term.

$$\begin{aligned} 30 \quad \frac{d^2}{dt^2} c_y(n, t) + \frac{2}{\tau} \frac{d}{dt} c_y(n, t) + \omega_n^2 c_y(n, t) - \frac{2}{\pi n} [(-1)^n - 1] g_y(0, t) \\ + (-1)^n \frac{2l}{\pi n} \Gamma_{yz}(0, t) \\ \pm \frac{1}{\eta} \frac{\mu_0}{2\pi^2 d} \epsilon_n I_0 I_y(z, t) \sin(\Omega t) \\ + \frac{2}{\eta l} \int_0^l dz \tilde{f}_L(z, t) \sin\left(\frac{\pi n}{l} z\right) \end{aligned} \quad (8)$$

35 The quantity ϵ_n relates to the characteristics of the transducer system of the feedback loop; the longer the length of the arms of the feedback circuit, the larger

- 16 -

the quantities e_n are. If the arms of the feed-back circuit are absolutely identical then the quantities e_n are equal to zero for all odd $n = 1, 3, 5, \dots$. Their particular values for the sizes shown in FIG.2 are
 5 determined by

$$e_n = \frac{1}{n} \left[\cos\left(\frac{\pi n}{6}\right) \cdot \cos\left(\frac{5\pi n}{6}\right) - 2 \cos\left(\frac{\pi n}{2}\right) \right] \quad (9)$$

So, for the properly adjusted feed-back circuit, only
 10 the antisymmetric natural modes of the string interact with the feed-back current. However, only the antisymmetric natural modes of the string are sensitive to the absolute value of the gravity gradient tensor component to be measured, as is seen from Eq.(4) and
 15 (7).

The superconducting pick-up coils L_{p1} and L_{p2} are placed near the string and cause two arms of the superconducting magnetic flux transformer to convert, if
 20 perfectly balanced, only the antisymmetric natural modes into the signal current I_i to be detected with the SQUID's electronics 13 (see FIG. 1). One uses SQUID's (Superconducting Quantum Interference Devices) 13 as they are the most sensitive variable current and
 25 magnetic flux sensors currently available. In the prototype shown in FIG.2, the pick-up coils are made in the form of two rectangular-type single loops of Nb wire placed symmetrically with respect to the midpoint of the string and connected in parallel with the signal coil L_i .
 30 If the symmetry is perfect and the areas of the loops are absolutely identical, then the symmetric natural modes do not produce any signal current I_i or feed-back current I_f . The same effect can be achieved for slightly non-identical pick-up coils with the accuracy required,
 35 if one uses the additional inductance(s) L_b connected in parallel and/or series with one or both of the pick-up coils. The inductance(s) L_b can be tuned to balance the two arms of the superconducting flux transformer. The

- 17 -

residual "zero-mode" current in the signal coil L_1 corresponding to the unperturbated position of the string can be compensated directly inside the SQUID by an additional coupling (not shown) to the pumping current source. If the balancing conditions are satisfied, then the output voltage of the SQUID's electronics 13 is determined by

$$V_y(t) = KI_0 L_s \sin(\Omega t) \left(\sum_{n=1}^{\infty} \beta_n c_y(n, t) \right) + K\Phi_N(t) \quad (10)$$

where K is the total flux to voltage transfer function and L_s is the SQUID's inductance. The quantities β_n depend on the physical design and position of the pick-up coils and are equal to zero if $n = 1, 3, 5, \dots$. The function $\Phi_N(t)$ is the equivalent-to-noise random magnetic flux inside the SQUID loop, whose spectral density $S_\Phi(\omega)$ determines the intrinsic instrumental limit of the accuracy of measurements. The feed-back current $I_y(t)$ is formed from the output voltage $V_y(t)$ by passing it through a differentiating and summing amplifier 16 which is loaded by resistance R_y . In this case, the feed-back current $I_y(t)$ can be represented by

$$I_y(t) = \frac{p\tau^*}{R_y} \frac{d}{dt} V_y(t) + \frac{q}{R_y} V_y(t) \quad (11)$$

where p , q and τ^* are constant parameters which depend upon the design of the differentiating and summing amplifier 16.

It must be noted that a mismatch between the two arms of the feed-back circuit always exists. The design shown in FIG.2 uses two identical feed-back resistances, R_{y1} and R_{y2} , one for each arm. In this case the mismatching can be easily compensated by tuning one of the resistances, say R_{y2} , to obtain the optimum case.

Equations (7) and (11) represent a closed infinite set of differential parametric-type equations. Careful

- 18 -

analysis has shown that we can ignore the terms involving the quantities $c_y(n, t)$ with $n > 2$ in the right-hand side of Eq. (11). The reason is that just one mode can be made "soft" i.e. the most sensitive to the gravity gradient, namely $c_y(2, t)$. If the string's natural frequencies are high enough and separated by single octave gaps, only second-order corrections are required which can be easily taken into account along with analysis of other instrumental errors. Then, as follows from Eq. (7), the self-consistent equation for the gravity gradient sensitive mode, $n=2$, including unavoidable fundamental noise sources can in turn be written in the form

$$\begin{aligned} \frac{d^2}{dt^2} c_y(2, t) + \left(\frac{2}{\tau} - \frac{1}{2} \alpha + \frac{1}{2} \alpha \cos(2\Omega t) \right) \frac{d}{dt} c_y(2, t) + \left(\omega_2^2 - \frac{1}{2} \bar{\omega}^2 + \frac{1}{2} \bar{\omega}^2 \cos(2\Omega t) - \frac{1}{2} \alpha \Omega \sin(2\Omega t) \right) c_y(2, t) - \frac{1}{\pi} \Gamma_{yz}(0, t) + \frac{2}{\eta l} \int_0^1 dz \tilde{f}_L(z, t) \sin\left(\frac{2\pi}{l} z\right) + (\text{back-action noise}) \sin(\Omega t) \end{aligned} \quad (12)$$

where

$$\bar{\omega}^2 = |e_2 \beta_2 q K| \frac{1}{\eta} \frac{\mu_0 I_0^2 L_s}{2\pi^2 d R_y} \quad \alpha = \bar{\omega}^2 \left| \frac{p}{q} \right| \tau \quad (13)$$

and it is assumed that the true sign of the feed-back current has been chosen.

If some easily carried out conditions are satisfied, which are

$$\frac{1}{\Gamma} \frac{d\Gamma}{dt} \ll \sqrt{\omega_2^2 - \frac{1}{2} \bar{\omega}^2} \quad 8\Omega^2 \gg \omega_2^2 \quad \frac{2}{\Omega \tau} \ll 1 \quad (14)$$

then one can show that the self-consistent output voltage is

$$V_y(t) = \beta_2 K I_0 L_s \left(\frac{1}{\pi} \frac{\Gamma_{yz}(0, t)}{\omega_2^2 - \frac{1}{2} \bar{\omega}^2} + \text{brownian noise} \right) \sin(\Omega t) + K \Phi_N(t) \quad (15)$$

- 19 -

where under "brownian noise" the combination of thermal and back-action noises is implied.

It is of interest to estimate the limiting accuracy of measurements of this embodiment of the invention, which can be represented by the value of a minimum detectable gravity gradient

$$\Gamma_{\min} = \frac{\pi}{l} \sqrt{\frac{16k_B T}{m\tau_{\text{eff}}} \cdot \frac{\bar{\omega}^4}{2\beta_2^2} \frac{E_\Phi(\Omega)}{L_s I_0^2}} 10^9 \frac{\text{Eötvös}}{\sqrt{\text{Hz}}} \quad (16)$$

where $\tau_{\text{eff}} = \tau/(1-\alpha\tau/4)$ is the effective relaxation time, m is the total mass of the string, and $E_\Phi(\Omega)$ is the energy resolution of the SQUID. Using the following practical parameters: $l=0.24\text{m}$, $m=1.6 \cdot 10^{-3} \text{ kg}$, $\tau_{\text{eff}}=10^4 \text{ s}$, $\beta_2=4 \times 10^3 \text{ m}^{-1}$, $L_s=5 \times 10^{-11} \text{ H}$, $I_0=50 \text{ A}$, $(\omega_2^2 - \omega^2/2)^{1/2}/2\pi=2 \text{ Hz}$, $\omega_2/2\pi=40 \text{ Hz}$, $\Omega/2\pi \geq 2 \times 10^2 \text{ Hz}$, $E_\Phi(\Omega)=2 \times 10^{-31} \text{ J/Hz (d.c. biased SQUID)}$, one can obtain from Eq. (16)

$$\Gamma_{\min} = 0.4 \frac{\text{Eötvös}}{\sqrt{\text{Hz}}} \quad (17)$$

It can be shown, that a range of the parameters τ , ω_2 , ω , α and Ω exists where the string's response described by Eq. 12 is stable. For example, for quasistatic gravity gradients and sufficiently high pumping frequency Ω one can ignore the oscillating terms containing $\text{Cos}(2\Omega t)$ and $\text{Sin}(2\Omega t)$ in the right side of Eq. 12.

There are a number of detecting strategies which can be employed by the present invention at this stage, which are dependent on the initial mechanical parameters of the string and the application for which the apparatus is intended. It is preferable to use a string with a high mechanical stiffness and a short relaxation time in order to increase immunity to vibrational noise, which is the main noise source in industrial applications, particularly in mobile gravity gradiometry. On the

other hand, the stiffer the string, the stronger the feedback force that has to be applied to the string to soften the signal mode, and the larger the back-action noise associated with the feedback current.

5

Additionally, the shorter the string's relaxation time, the stronger the influence of thermal fluctuations of the string on the measuring accuracy since the mass per unit length of the string will normally be quite small.

10

To overcome both of these problems a best mode of carrying out gravity gradient measurements according to another embodiment of the present invention uses variable feedbacks in an "off-on" manner. In this case, the feedback force is initially not applied to the string for an 'off-period' during which the string reaches thermodynamic equilibrium. The feedback force is then quickly activated for an 'on-period' during which the effective natural frequency

20

$$\omega_{eff} = \sqrt{\omega_2^2 - \frac{1}{2}\bar{\omega}^2} \quad (18)$$

and the effective relaxation time

25

$$\tau_{eff} = \tau \left(1 - \frac{\alpha\tau}{4} \right)^{-1} \quad (19)$$

become substantially smaller and longer respectively compared to the corresponding initial parameters of the string. The feedback is adjusted in such a way that the effective relaxation time becomes much longer than the on-period. Measurements are carried out during the on-period only, in which the string never reaches thermodynamic equilibrium. For example, the fluctuation dissipation theorem is no longer applicable to the string during the period of measurements and its response to all external noise sources is changed (see V.B. Braginsky and A.B. Manukin, Measurement of Weak Forces in Physics Experiments, Ed. by D.H. Douglass,

35

- 21 -

University Press of Chicago, 1977).

One can show that in this case the least gravity
gradient detectable by this embodiment of the invention
5 can be represented by

$$\Gamma_{\min} = \frac{\pi}{l} \sqrt{\gamma(\delta) \frac{16k_B T}{m \tau \tau_m} \cdot \frac{\bar{\omega}^4}{2\beta_2^2 L_s I_0^2 \tau_{\text{eff}}} \log\left(\frac{1}{\delta}\right)} 10^9 \text{ Eötvös} \quad (20)$$

10

where

$$\gamma(\delta) = \frac{4\tau \tau_m}{\tau_{\text{eff}}^2} \log\left(\frac{1}{\delta}\right) + \frac{\omega_{\text{eff}}^4}{\omega_2^4} \left[\frac{1}{\delta} + \log\left(\frac{1}{\delta}\right) \right] \quad (21)$$

15

τ_m is the measurement time (on-period), m is the total mass of the string, $E_\Phi(\Omega)$ is the energy resolution of the SQUID at the frequency Ω and δ is a statistical error of the first kind. The value of δ is the likelihood that
20 the equivalent gravity gradient noise will exceed the value represented by the left side of Eq. 20 for the period of measurement.

Using the following practical parameters: $l=0.24$ m,
25 $m=1.6 \times 10^{-3}$ kg, $\tau=0.5$ s, $\tau_m=1$ s, $\tau_{\text{eff}}=10^4$ s, $\beta_2=4 \times 10^3$ m⁻¹,
 $L_s=5 \times 10^{-11}$ H, $I_0=50$ A, $\omega_{\text{eff}}/2\pi=3$ Hz, $\omega_2/2\pi=80$ Hz, $\Omega/2\pi \geq 10^4$ Hz, $E_\Phi(\Omega)=5 \times 10^{-32}$ J/Hz (500h d.c. biased SQUID), one can obtain from Eq. (20)

30

$$\Gamma_{\min} = 0.02 \text{ Eötvös}$$

In both the above embodiments, the desired signal is obtained from the output voltage by synchronous detection with a reference signal taken from the pumping
35 source 15, and the invention allows calibration of the desired signal in gravity gradient absolute units without rotation as has been proposed for known rotating gravity gradiometers. As for rotating designs, the

- 22 -

invention allows the movement of the noise spectrum to a frequency range at which $1/f$ contribution is sufficiently small. Natural vibrations of the string, which occur during the time of measurement (on-period),
5 do not cause a problem since they can be filtered out from the desired signal provided that the on-period is chosen to be much longer than the period ($2\pi/\omega_{\text{eff}}$) of such vibrations.

10 Vibrational noise immunity is improved by the factor $(\omega_{\text{eff}}/\omega_1)^2$ which can be made as small as 10^{-2} .

One must consider inductive cross-coupling between the feedback currents and each pair of the pick-up coils and
15 cross-coupling between the pick-up coils themselves, both of which act like negative feedback loops. On the one hand this leads to unnecessary renormalisation of the amplitudes of the output signals until the gain of the SQUID's electronics exceeds some critical value. On
20 the other hand in the case of double-channel measurements, the output signal of each channel contains a linear combination of each gravity gradient component to be measured. It can be shown that each of such components can, nevertheless, be measured separately and
25 simultaneously, if a proper data acquisition system is used. The effect can be easily eliminated by organising additional positive feedback to counteract this negative feedback, for example by connecting, via a weak inductive coupling, each feedback current with each
30 SQUID.

In practice, the apparatus according to the invention can be used to determine in absolute units the off-diagonal components of the gravity gradient. By
35 conducting a gravity survey over an area, small differences in absolute gravity gradient can be detected. Such small changes may indicate variations in local geological features, for example, the presence of

minerals, gas or oil.

Repeated readings over time at a single locality could indicate changing geological status of an area, such as rising magma. Clearly the invention enhances prospecting and other data gathering pursuits where accurate gravitational field measurement is required. Use of absolute values enhances the information that can be determined from the data measured. A gradiometer according to the invention can be used while moving, which allows the gradiometer to be used on vehicles whether land, sea or air vehicles. For example, the device can be suspended from a helicopter and used while the helicopter traverses a selected area.

Claims

1. Apparatus for the measurement of quasi-static gravitational fields, comprising:
 - 5 a string fixed at both ends and held under tension; sensing means for detecting the transverse displacement of said string from an unperturbated position due to a gravitational field acting on said string; and
 - 10 means responsive to the detected displacement for producing an output which is a function of the gravitational field.
2. Apparatus as claimed in claim 1, wherein said
15 sensing means comprises at least two sensors symmetrically longitudinally positioned about the mid-point of said string.
3. Apparatus as claimed in claim 1 or 2, wherein said
20 string is composed of conductive material and carries a current I_0 .
4. Apparatus as claimed in claim 3 further comprising
25 conductive means adjacent said string carrying a current I_y , wherein the magnitude of the current I_y is a function of the output of the sensing means; and the magnetic fields associated with the current I_y through the conductive means and the current I_0 through the string
30 interact to produce a feedback force on said string so as to increase the transverse displacement of the string from its unperturbated position in response to the gravitational field acting on said string.
5. Apparatus as claimed in claim 4, wherein said
35 conductive means comprises at least two conductors longitudinally symmetrically positioned about the mid-point of said string, each conductor carrying a substantially equal proportion of said current I_y .

- 25 -

6. Apparatus as claimed in claim 4 or 5 wherein the current I_y through said conductive means is activated periodically.

5 7. Apparatus as claimed in any of claims 3 to 6, wherein said sensing means comprises at least one pick-up coil in which a current I_p is induced by said current I_o through said string, said current I_p being a function of said string's displacement.

10 8. Apparatus as claimed in any of claims 3 to 7, wherein said current I_o through said string is an alternating current.

15 9. Apparatus as claimed in any of claims 3 to 8 wherein said current I_o is induced in said string by inductive means.

20 10. Apparatus as claimed in claim 9, wherein said inductive means comprises two solenoids longitudinally symmetrically positioned about the mid-point of said string.

25 11. Apparatus as claimed in any of claims 3 to 10, wherein said string is composed of superconducting material.

30 12. Apparatus as claimed in any preceding claim, wherein said sensing means comprises means for detecting the transverse displacement of said string in two non-parallel planes.

35 13. Apparatus for measuring off-diagonal components of the gravity gradient tensor comprising a flexible string having fixed ends, means to apply a force per unit length to said string so that deflection of said string is caused by absolute values of transverse-to-string components of said force, in a manner such that

- 26 -

deflection of said string is a combination of said string natural modes, and the even said modes are caused only by absolute values of the components of the gravity gradient in the string direction, whilst the odd said
5 modes are caused by total acceleration in the transverse-to-string plane.

14. A method of measuring quasi-static gravitational fields, comprising:

10 providing a string with fixed ends and held under tension;

detecting the transverse displacement of said string from an unperturbated position due to a gravitational field acting on said string; and

15 producing an output in response to the detected displacement, said output being a function of said gravitational field.

15. A method as claimed in claim 14 wherein said output
20 is produced by measuring the spatial position of at least one point on the string relative to the unperturbated position of said point.

16. A method as claimed in claim 15 wherein the spatial
25 positions of an even plurality of points on the string are measured relative to their unperturbated positions and said points are chosen to lie pair-wise longitudinally symmetrically about the mid-point of the string.

30 17. A method as claimed in claim 16 wherein said points correspond to the positions of antinodes of the antisymmetric natural modes of said string.

35 18. A method as claimed in any of claims 14 to 17 wherein said displacement of said string is increased by applying a feedback force to the string, said force being a function of the gravitational field acting on

the string.

19. A method as claimed in claim 18 wherein said feedback force is a direct function of said output.

5

20. A method as claimed in claim 19 wherein said feedback force is applied to said string so as to accentuate the components of the spatial configuration of the string corresponding to natural antisymmetric modes of the string in preference to the components of the spatial configuration corresponding to natural symmetric modes.

10

21. A method as claimed in any one of claims 14 to 19 wherein said displacement is measured in two non-parallel planes.

15

22. A method of measuring absolute off-diagonal components of the gravity gradient tensor by means of a flexible string with fixed ends whose deflection from its unperturbed position is caused by absolute value of transverse-to-string components of a force per-unit-length applied to each unit element of said string in a manner that said deflection is a combination of said string's natural modes, and the even said modes are caused only by absolute values of the components of the gravity gradient in the string's direction, whilst the odd said modes are caused by total acceleration in the transverse-to-string plane.

20

25

30

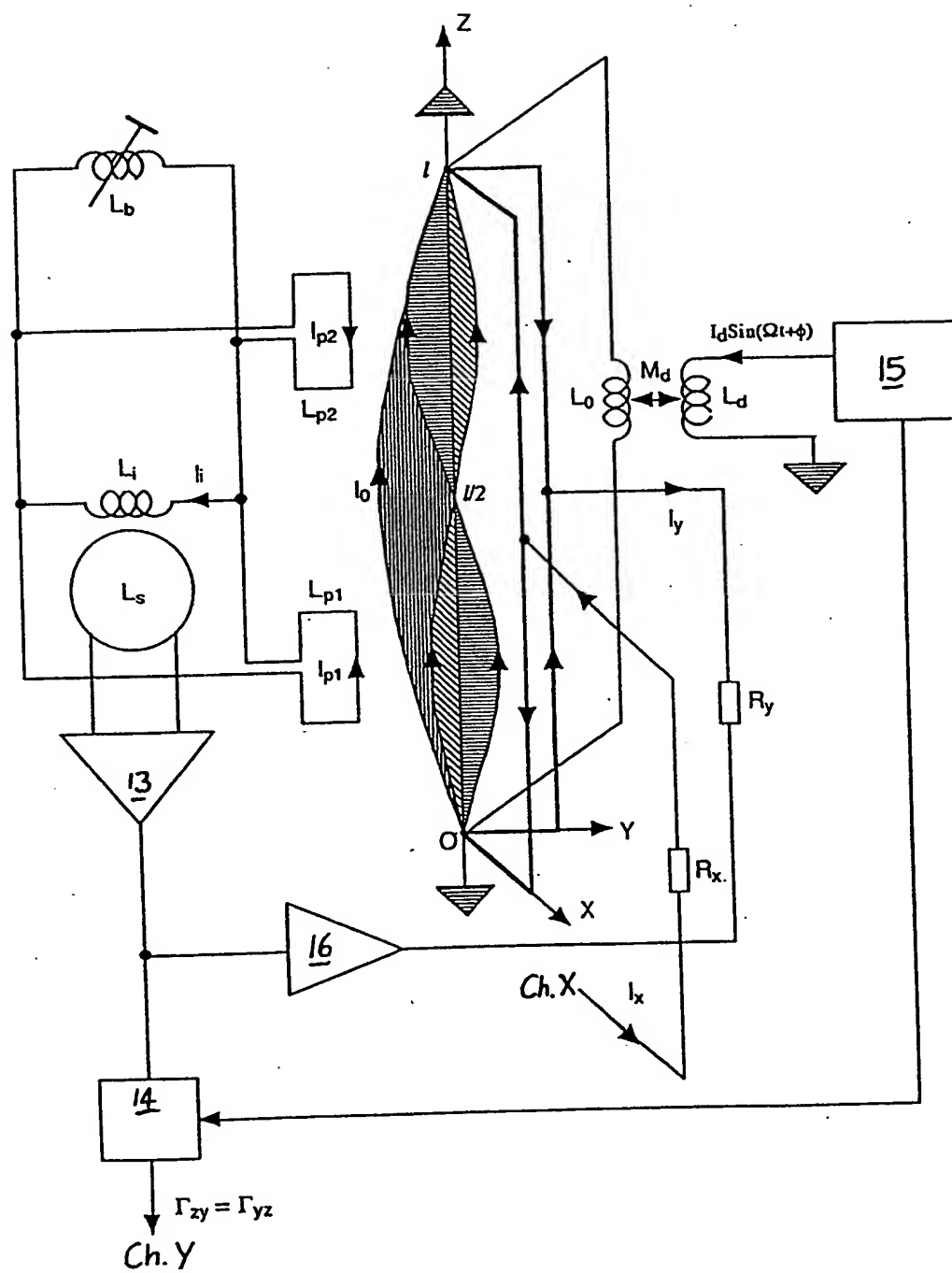


Fig. 1

2/2

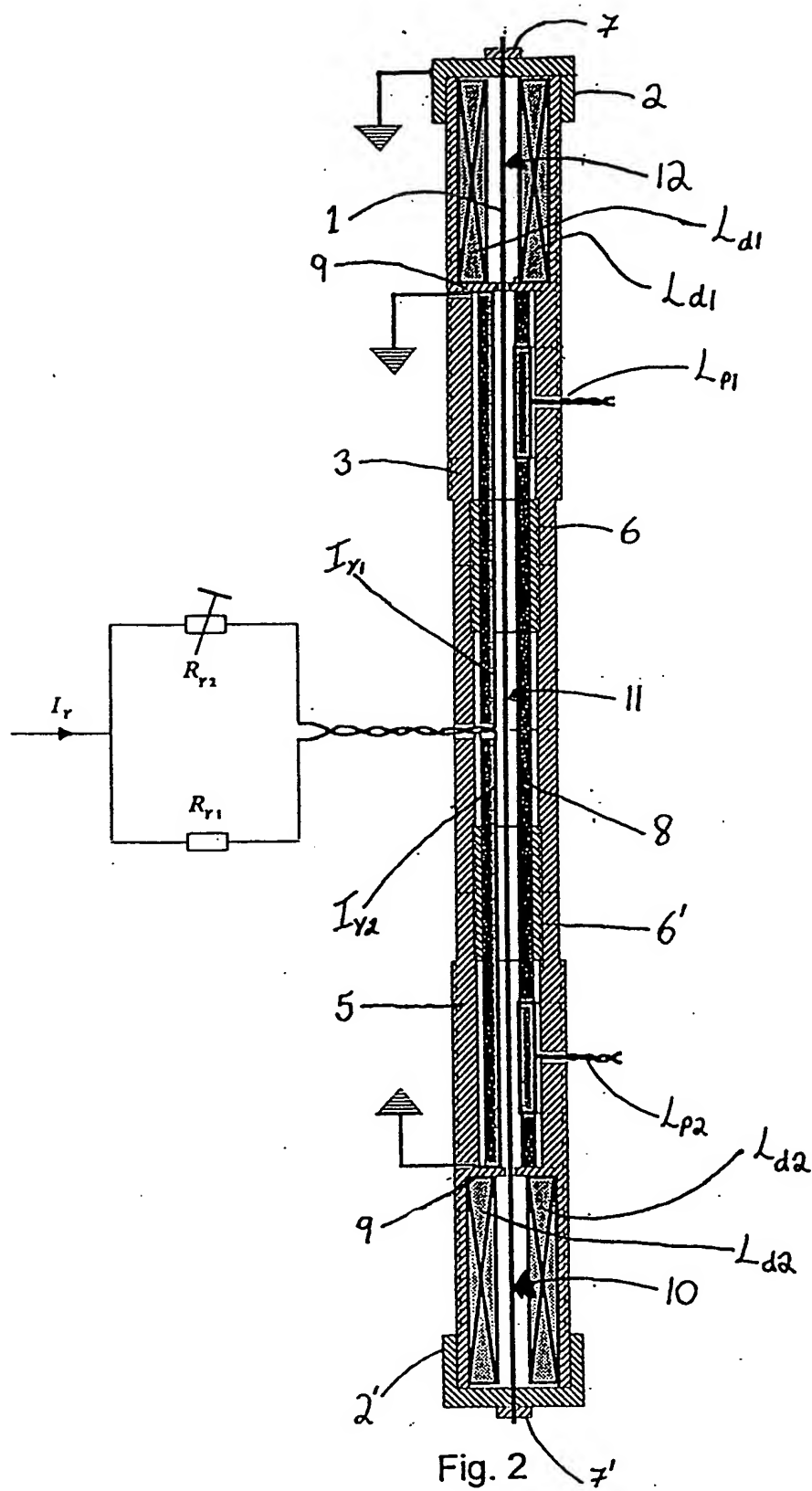


Fig. 2

INTERNATIONAL SEARCH REPORT

Intern al Application No
PCT/GB 95/02349

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>NUOVO CIMENTO B, NOV. 1992, ITALY, vol. 107B, ser.2, no. 11, ISSN 0369-3554, pages 1261-1265, NICOLAIDIS A ET AL 'String as a gravitational antenna' cited in the application ---</p>	1
A	<p>US,A,3 722 284 (FORWARD R ET AL) 27 March 1973 cited in the application ---</p>	
A	<p>US,A,3 769 840 (HANSEN S) 6 November 1973 cited in the application ---</p>	
A	<p>US,A,3 564 921 (BELL CURTIS C) 23 February 1971 cited in the application ---</p>	
A	<p>WO,A,89 05462 (UNIV MARYLAND) 15 June 1989 cited in the application -----</p>	

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No
PCT/GB 95/02349

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A-3483753	16-12-69	NONE	
US-A-2657581	03-11-53	NONE	
US-A-3722284	27-03-73	NONE	
US-A-3769840	06-11-73	NONE	
US-A-3564921	23-02-71	CH-A- 499116	15-11-70
		DE-A- 1805048	14-08-69
		FR-A- 1591216	27-04-70
		GB-A- 1219165	13-01-71
		NL-A- 6815655	05-08-69
WO-A-8905462	15-06-89	US-A- 4841772	27-06-89
		AU-B- 3191089	05-07-89
		CA-A- 1321482	24-08-93